



Lecture 10 - Accident Analysis

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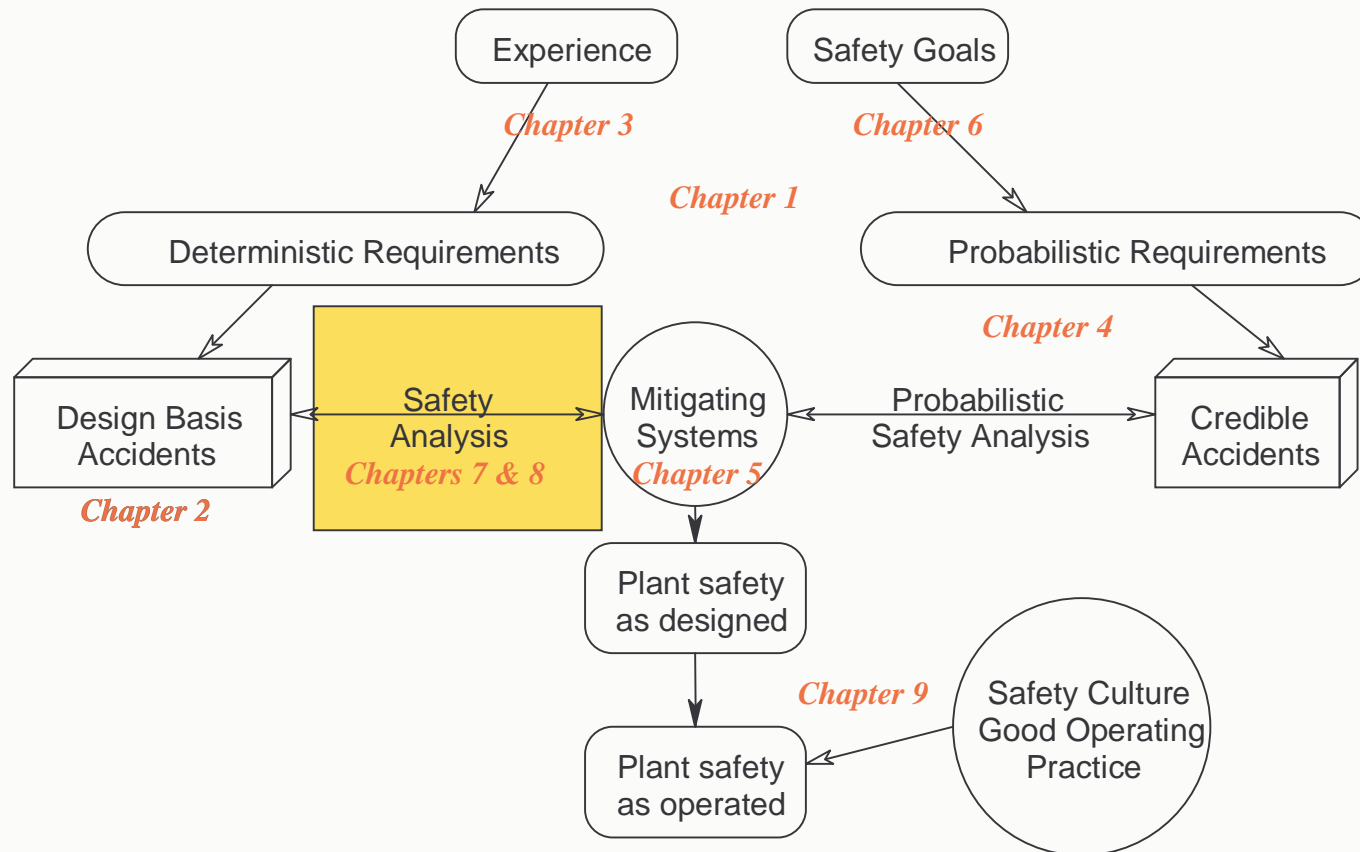
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Where We Are





Severe Accidents

- Beyond Design Basis Accidents
 - core geometry is preserved
 - fuel may be damaged but remains inside intact pressure tubes
- Severe core damage accidents
 - fuel channels fail and collapse to the bottom of the calandria

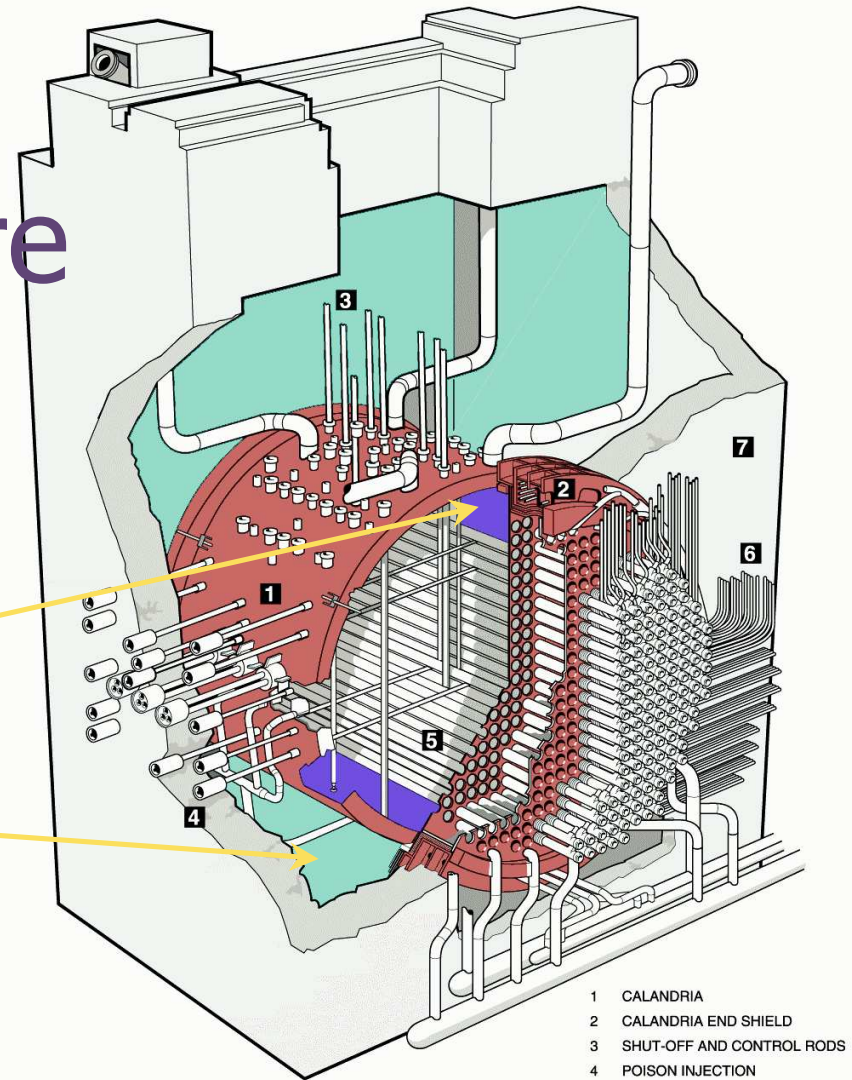


Examples

- Loss of coolant + Loss of Emergency Core Cooling (BDBA)
- Loss of all secondary side heat sinks + Loss of shutdown cooling system, moderator available (BDBA)
- Loss of coolant + Loss of Emergency Core Cooling + Loss of moderator heat removal (SCDA)

Water Near Core

<i>System</i>	<i>Continuous Heat Removal Capability (% full power)</i>	<i>Time to heat up and boil off, no heat removal</i>
<i>Moderator</i>	4.4%	> 5 hours
<i>Shield Tank</i>	0.4%	10 to 20 hours



- 1 CALANDRIA
- 2 CALANDRIA END SHIELD
- 3 SHUT-OFF AND CONTROL RODS
- 4 POISON INJECTION
- 5 FUEL CHANNEL ASSEMBLIES
- 6 FEEDER PIPES
- 7 VAULT

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CANDU 6 Reactor Assembly



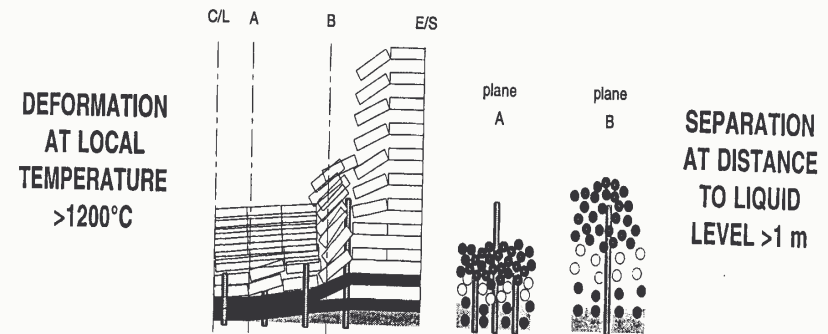
Loss of Core Geometry - 1

- E.g., Loss of all heat sinks + inability to depressurize HTS
- Pressure rises to relief valve setpoint
- Loss of water through relief valves
- Overheating of fuel and pressure-tubes at high pressures
- Failure of a few pressure tubes (6-10 MPa) – depressurize HTS

Loss of Core Geometry - 2

- Remaining pressure tubes strain to contact calandria tube
- Boil-off of moderator
- Sag & failure of channels at *low* pressure at $\sim 1200^{\circ}\text{C}$ as moderator level falls
- Collapse of channels onto lower neighbours

UNCOVERED CHANNELS DEFORM BY SAGGING
SEGMENTS SEPARATE BY MEMBRANE STRETCHING
WHEN SUFFICIENT DEFLECTION DISTANCE AVAILABLE



SUBMERGED CHANNELS FAIL AT ROLLED JOINT WHEN
SUFFICIENT DEBRIS LOAD BUILDS UP (CORE COLLAPSE)

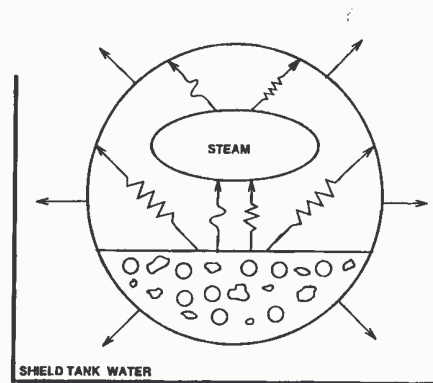


Characteristics of Debris Bed

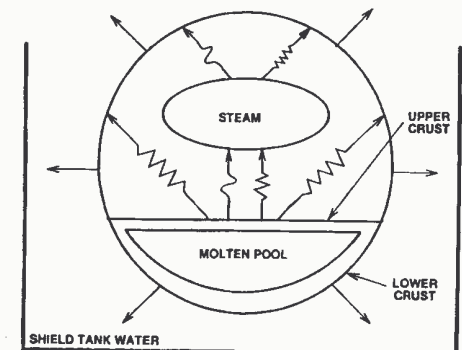
- Top channels collapse when moderator is half voided, so they sag into a pool of water
- Debris likely to be composed of coarse pieces of ceramic materials
- Bed will not be molten until all the moderator water is boiled off - will then dry out and heat up due to decay heat & remaining Zircaloy-steam reaction
- No energetic fuel-coolant interaction
- No criticality, even for ACR
- Models for heat transfer from debris bed to calandria walls developed by T. Rogers et al. for dry debris, and also debris with molten centre

Debris Bed Models

- Uniform porous mixture of UO_2 , ZrO_2 and/or Zircaloy
- Fuel decay heat + metal water reaction
- Thermal radiation to inner surface of calandria from top of the bed
- Conduction through bottom of calandria to shield tank water



a) Debris bed



b) Molten pool and crusts

———→ Natural convection or nucleate boiling to shield tank water
 ~~~~~→ Radiation  
 ~~~~~→ Natural convection

Debris Bed Heatup

- Melting of debris starts about 7 hours after the event
- Upper & lower surfaces of debris bed stay below melting temperature

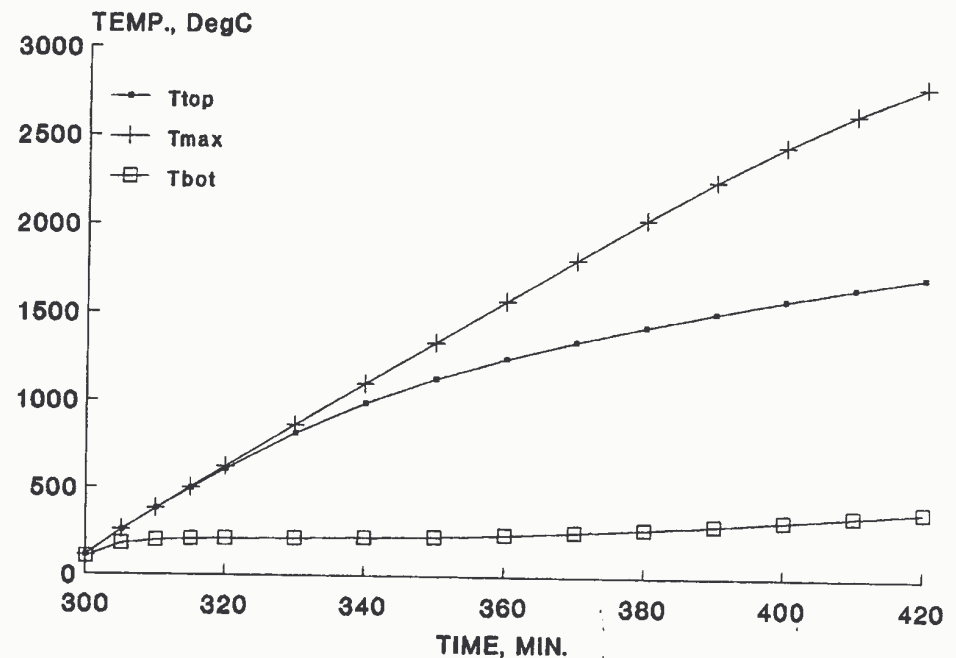
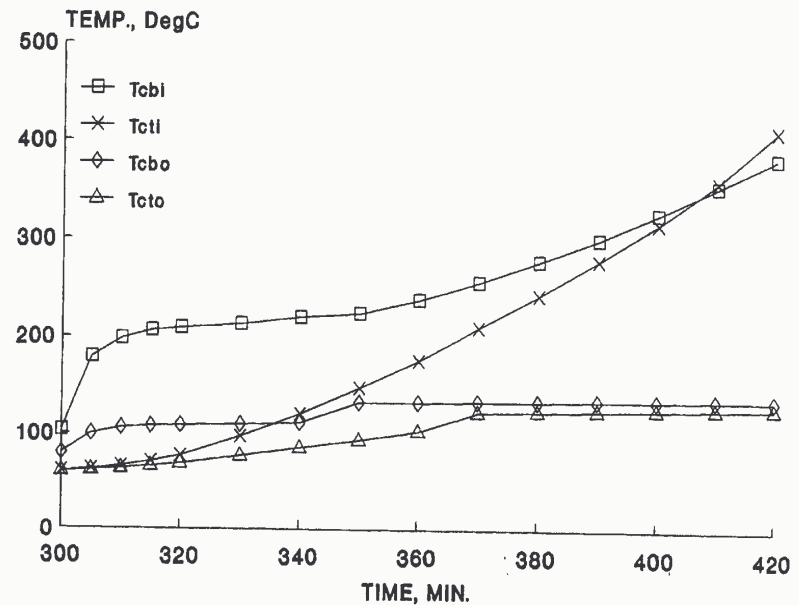


Figure 7 Heat Up of Core Debris in CANDU 6 Calandria, Reference Conditions

Calandria Wall Temperatures

- Outer surface temperature below 140C
- Stainless steel wall
- Do not expect creep under applied stresses



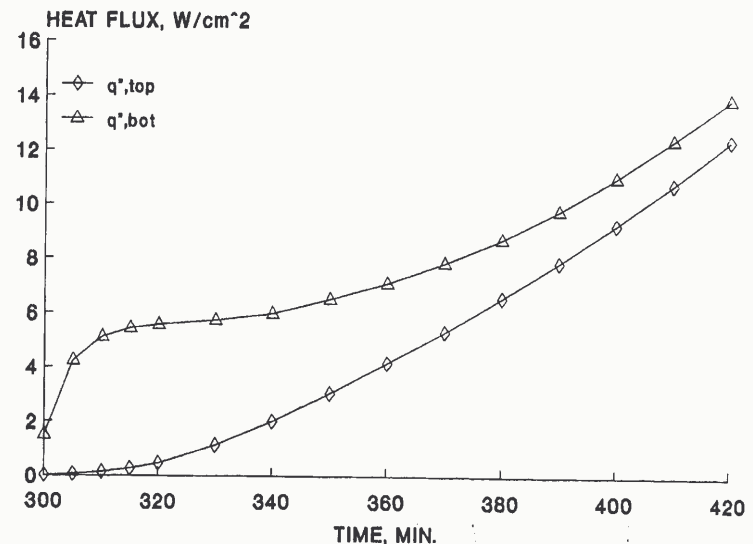
Porosity= 0.5, Pore Size= 3 cm

Figure 8 Calandria Wall Temperatures, Heat Up of Core Debris, CANDU 6 Calandria

Heat Flux to Shield Tank

- Heat flux to shield tank 15 times less than CHF
- Calandria will remain intact while shield tank water boils off
- Behaviour insensitive to porosity and timing of metal-water reaction

Critical heat flux
200 W/cm²



Reference Conditions
Porosity = 0.05, Pore Size = 3 cm

Figure 9 Heat Fluxes on Calandria Wall, Heat Up of Debris in CANDU 6 Calandria



Summary of Time-scales

| <i>Time (hr)</i> | <i>Event</i> |
|------------------|--|
| <i>0</i> | Loss of heat sinks, reactor shutdown |
| <i>0.75</i> | Steam Generators boil dry, liquid relief valves open, fuel cooling degrades |
| <i>0.83</i> | A few pressure tubes fail and depressurize heat transport system |
| <i>0.86</i> | High pressure ECC initiated; medium pressure ECC assumed to fail |
| <i>1.1</i> | Heat transport system empty |
| <i>5</i> | Moderator boiled off, channels sagged to bottom of calandria |
| <i>25</i> | Vault water boiled off to top of debris bed, calandria fails |
| <i>Days</i> | Interaction of debris with vault floor & penetration to containment basement |

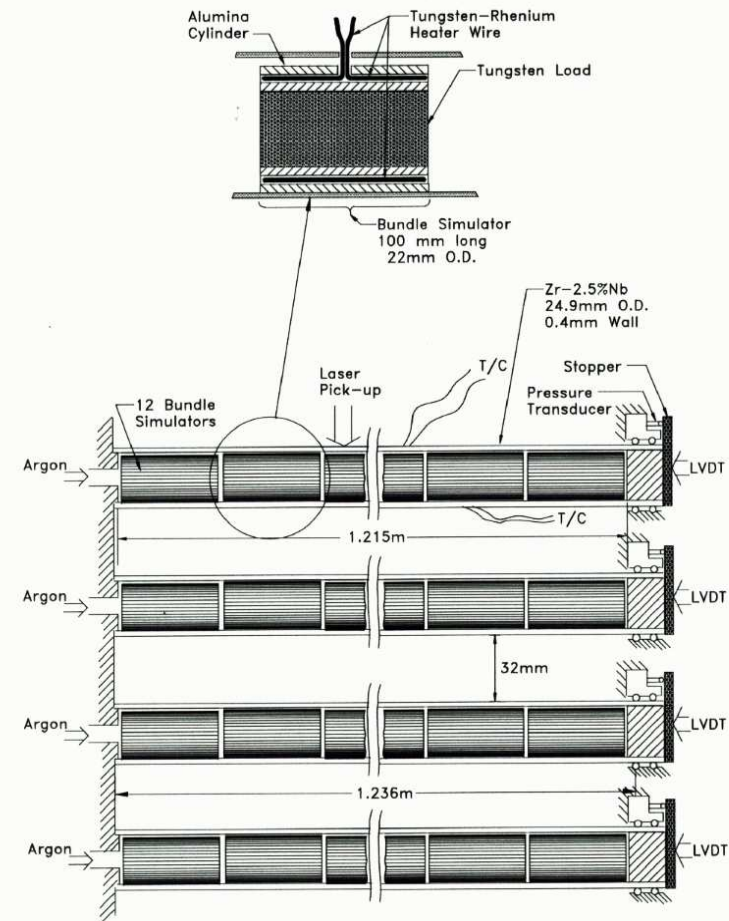


Uncertainties

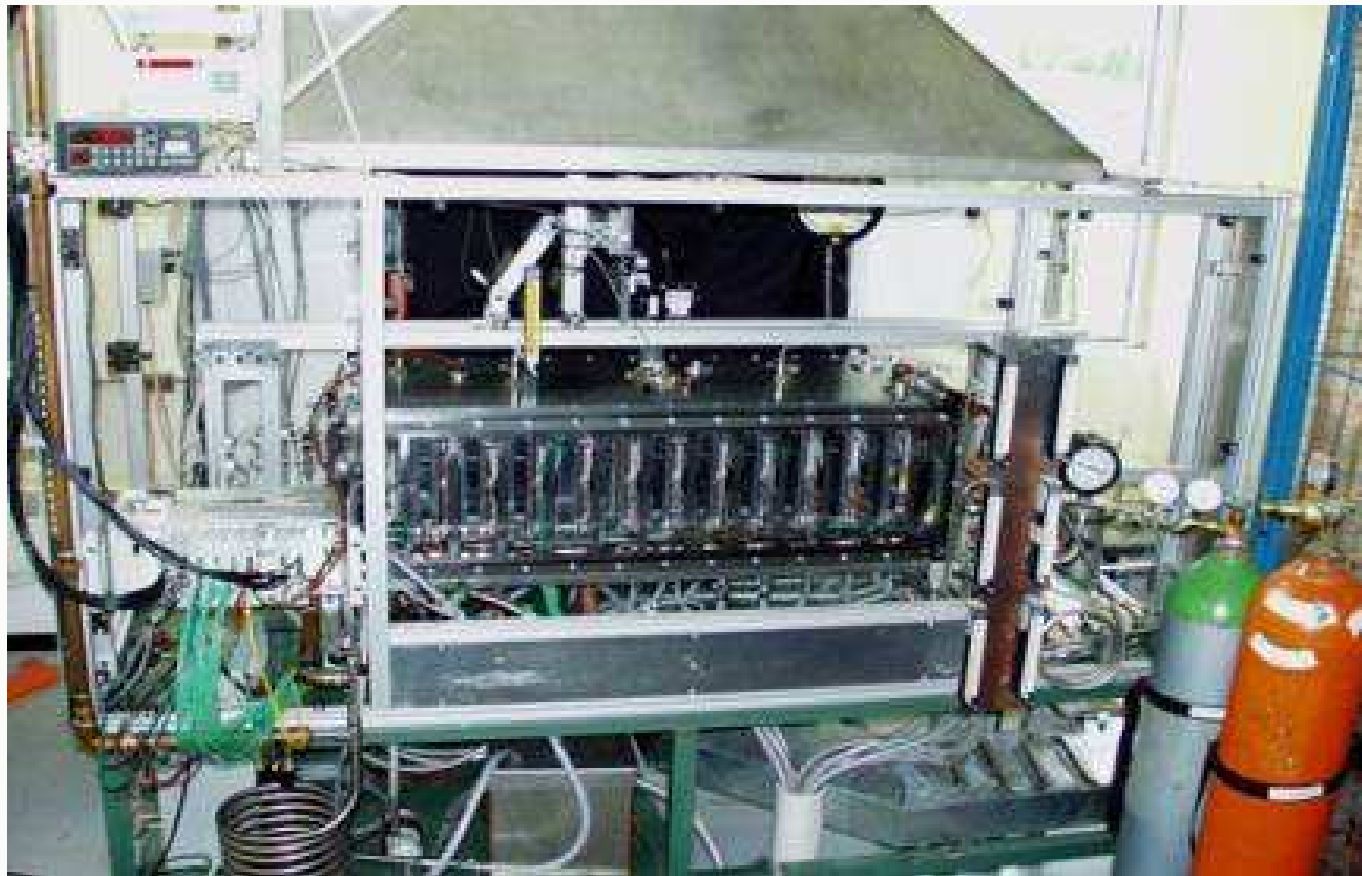
- Mechanical and thermal behaviour of end-shields
- Capability of shield tank to relieve steam
- Local effects in molten pool and hot-spots
- Lack of experimental validation of debris melting transient
- Demonstration of core collapse mode

Tests on Channel Collapse

- 1/5 scale study
- Scaling retains full size stress levels, ratio of bundle size to channel length and channel length to pitch height of assembly



Test Rig



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Channel Failure Mode



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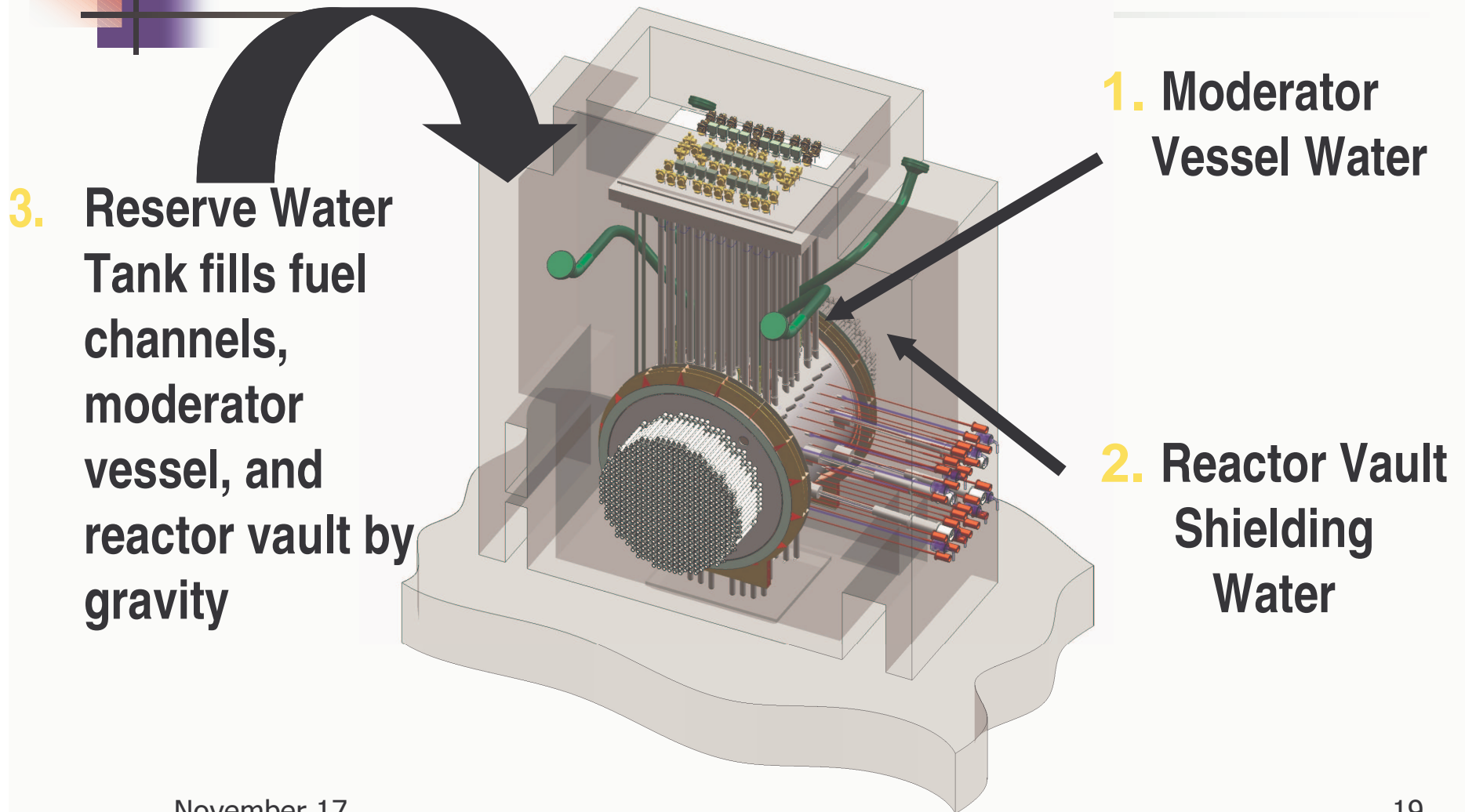
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Channel Collapse – Early Results

- Significant sag occurs only above 800C.
- Sag is creep-controlled
- PT wall thins at the bundle junctions - debris may be two to three bundles long
- The end-load is not sufficient to pull out the channel from the end-fitting

ACR Severe Accidents





Containment

- Containment heat removal (local air coolers) may or may not be available depending on the accident
- If not available, pressure initially controlled by dousing sprays
- With no heat sink, will eventually rise above design pressure
- Structure will remain intact due to leakage through cracks and pressure relief
- Mitigation: venting, dedicated heat removal chain, re-route LTC, firewater etc.



Observations

- Severe core damage in CANDU is very different from LWRs
- Low power density (16 MW/Mg of fuel at full power)
- Long heatup times (hours)
- Gradual collapse of the core into a coarse debris bed
- Dispersion of the debris in the large calandria
 - shallow molten pool about 1 metre deep
- Presence of two large sources of water in or near the core
- Potential to stop or slow down the accident at two points:
 - channel boundary (moderator)
 - calandria boundary (shield tank)
- Hydrogen control a necessity in short- and long-term



Coherent vs. Incoherent

LWRs

- Fuel melts rapidly (minutes) and “candles” down to the bottom of the vessel
- Vessel fails suddenly ejecting molten fuel
- Potential for steam explosion in vessel and in containment

CANDU

- Fuel melts slowly (hours) and slumps gradually down to the bottom of the vessel
- Vessel fails after a day; shield tank provides further barrier
- Continual steam release - explosion less likely



Severe Accident Conclusions

- Severe accident mitigation requirements for new reactors stress two design measures:
 - core debris spreading area
 - ability to add water to cool debris
- CANDU: calandria spreads the debris, and shield tank provides cooling water
- Long time scales allow for severe accident counter-measures and emergency planning
- Independent makeup to moderator and shield tank for EC6 and ACR
- Future: backup or passive containment heat removal



Uncertainty Analysis

- Disadvantages of conservative approach:
 - Overestimates / exaggerates risk
 - Misleadingly small margins
 - Useless as operator guide
 - Distorts safety resource allocation
- UA useful only with *best-estimate methods (BE+UA) – aka BEAU*



Types of Uncertainty

- Physical models
 - Model bias
 - Experimental scatter
 - Example: WIMS predicts coolant void reactivity for 37-element fuel with a bias of -1.6 mk. and an experimental uncertainty of ± 1 mk.
- Plant idealization
 - Example: How many spatial nodes for convergence?
- Plant data
 - Example: Uncertainty in flow measurement



Focus of Uncertainty Analysis

- UA stated only for key safety parameters output by the code & compared to acceptance criteria
 - E.g., peak fuel temperature
 - E.g., *not* internal parameter such as fission gas pressure



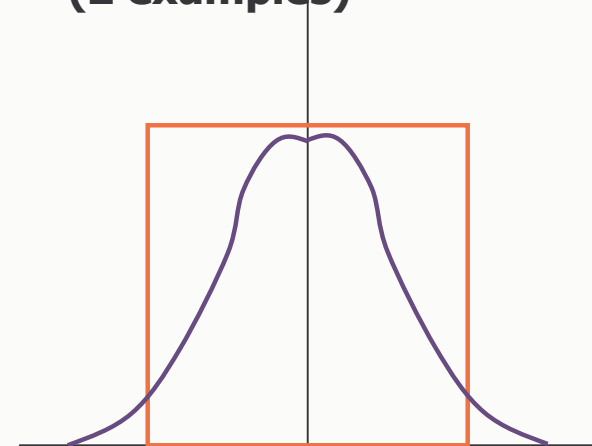
Issue

- Assume there are < 8 contributors to a key parameter
 - E.g., key parameter is fuel temperature in LOCA power pulse
 - Contributors are void reactivity, sheath-to-coolant heat transfer, delayed neutron fraction etc.
- Cannot afford to vary 8 simultaneously using fundamental codes
- Surrogate needed (curve fitting or functional form)

Simplified Methodology

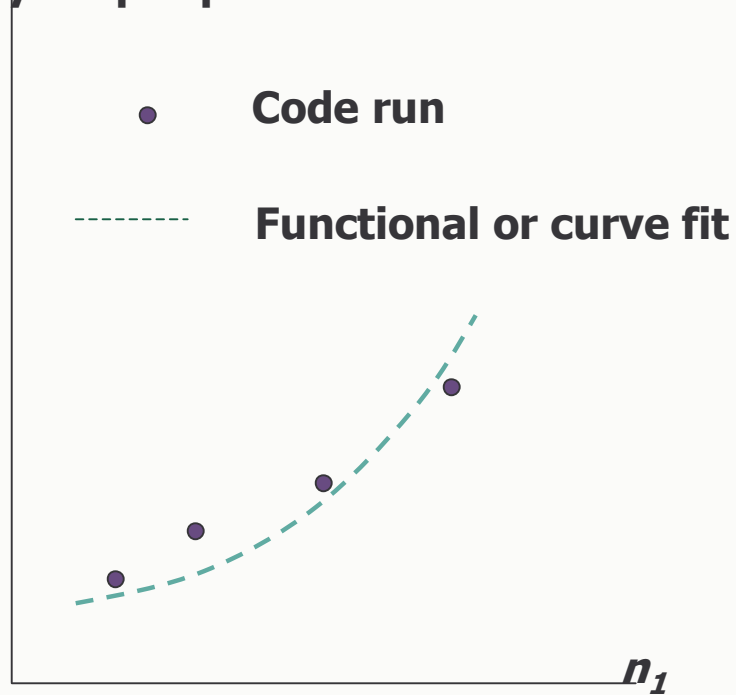
- Generate cases for variation of n contributory parameters using fundamental code
- Fit surface with functional form
- Test goodness of fit
- Sample surface based on statistical distribution of each parameter

Probability distribution of Contributory parameter (2 examples)



Graphical Example

Key output parameter



Key output parameter

