

ENGINEERING PHYSICS 4D3/6D3

DAY CLASS

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DURATION: 50 minutes

McMASTER UNIVERSITY MIDTERM EXAMINATION

November 9, 2000

Special Instructions:

1. Closed Book. All calculators and up to 8 single sided 8 ½" by 11" crib sheets are permitted.
 2. Do all questions.
 3. The value of each question is as indicated. TOTAL Value: 30 marks
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THIS EXAMINATION PAPER INCLUDES 1 PAGE AND 3 QUESTIONS. YOU ARE RESPONSIBLE FOR ENSURING THAT YOUR COPY OF THE PAPER IS COMPLETE. BRING ANY DISCREPANCY TO THE ATTENTION OF YOUR INVIGILATOR.

1. [10 marks] Given the material properties for a homogeneous fuel water mixture, ie specified Σ_a , $\nu\Sigma_f$ and D , a **cubic** reactor is proposed. It is calculated (using the simple one speed diffusion model) to go critical at dimensions $H \times H \times H$, where H is the side length.
 - a. What is the one speed steady state diffusion equation for the cubic reactor?
 - b. Given a flux shape of

$$\phi(x, y, z) = \phi_0 \cos\left(\frac{\pi x}{H}\right) \cos\left(\frac{\pi y}{H}\right) \cos\left(\frac{\pi z}{H}\right)$$

what is the criticality condition?

- c. What are the geometric and material bucklings? Are they equal?
2. [10 marks] Given the material properties for a homogeneous fuel water mixture, ie specified Σ_a , $\nu\Sigma_f$ and D , a **cylindrical** reactor is proposed. It is calculated (using the simple one speed diffusion model) to go critical at dimensions $R \times H$, where R is the radius and H is the height. The cylindrical reactor has the optimal shape that you determined in a recent assignment:

$$\frac{\text{Radius}}{\text{Height}} = \frac{2.405}{\sqrt{2\pi}}$$

- a. What is the one speed steady state diffusion equation for the cylindrical reactor?
 - b. Given a flux shape of
- $$\phi(r, z) = \phi_0 J_0\left(\frac{v_0 r}{H}\right) \cos\left(\frac{\pi z}{H}\right), \text{ where } v_0 = 2.405$$
- c. What are the geometric and material bucklings? Are they equal?
- what is the criticality condition?
3. [10 marks] For the two reactor models presented in the previous questions (one cubic in shape, the other cylindrical in shape):
 - a. Compare the bucklings. Are they equal?
 - b. Does the cubic reactor require more or less fuel water mixture than a cylindrical shaped reactor for criticality?
 - c. If both reactors were operating at the same total power level, compare the flux levels. Are they equal?
 - d. Compare the rates at which both reactors burn up fuel. Are they equal?

---The End---

Solution

1. a) $\frac{1}{\nu} \frac{\partial^2 \phi}{\partial z^2} = \nabla \cdot D \nabla \phi + (\nu \Sigma_f - \Sigma_a) \phi \Rightarrow D \nabla^2 \phi + (\nu \Sigma_f - \Sigma_a) \phi = 0$
 ↑ not a function of space

$\Rightarrow \nabla^2 \phi + \left(\frac{\nu \Sigma_f - \Sigma_a}{D} \right) \phi = 0 \Rightarrow \nabla^2 \phi + B^2 \phi = 0$ ①

where $\nabla^2 \phi = \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2}$ ↑ Buckling

b) $\phi = \phi_0 \cos\left(\frac{\pi x}{H}\right) \cos\left(\frac{\pi y}{H}\right) \cos\left(\frac{\pi z}{H}\right)$

Sub into ①: $-\left(\frac{\pi}{H}\right)^2 - \left(\frac{\pi}{H}\right)^2 - \left(\frac{\pi}{H}\right)^2 + B^2 = 0$

$\therefore B^2 = 3\left(\frac{\pi}{H}\right)^2 = \frac{\nu \Sigma_f - \Sigma_a}{D} = \text{criticality condition}$

c) $B_g^2 = \text{geometric buckling} = \left(\frac{3\pi}{H}\right)^2$
 $B_m^2 = \text{material buckling} = \frac{\nu \Sigma_f - \Sigma_a}{D}$ } equal criticality

2. a) as per 1. above except $\nabla^2 \phi = \frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \phi}{\partial r} + \frac{\partial^2 \phi}{\partial z^2}$
 $\nabla^2 \phi + B^2 \phi = 0$ as before
 $B^2 = \frac{\nu \Sigma_f - \Sigma_a}{D}$ as before.

b) $\phi = \phi_0 J_0\left(\frac{\nu_0 r}{H}\right) \cos\left(\frac{\pi z}{H}\right)$, $\nu_0 = 2.405$

Sub in as before: $-\left(\frac{\nu_0}{R}\right)^2 - \left(\frac{\pi}{H}\right)^2 + B^2 = 0$

$\therefore B^2 = \left(\frac{\nu_0}{R}\right)^2 + \left(\frac{\pi}{H}\right)^2 = + \left(\frac{\nu_0}{\frac{R}{\sqrt{2}\pi}}\right)^2 + \left(\frac{\pi}{H}\right)^2 = + \left(\frac{\sqrt{2}\pi}{H}\right)^2 + \left(\frac{\pi}{H}\right)^2 = 3\left(\frac{\pi}{H}\right)^2$
 $= \frac{\nu \Sigma_f - \Sigma_a}{D} \Leftarrow \text{criticality condition}$

$$c. \left. \begin{aligned} B_g^2 &= \left(\frac{v_0}{R}\right)^2 + \left(\frac{\pi}{H}\right)^2 = 3\left(\frac{\pi}{H}\right)^2 \\ B_m^2 &= \frac{\nu \Sigma_f - \Sigma_a}{D} \end{aligned} \right\} \text{equal at} \\ \text{criticality}$$

3. Cubic reactor vs cylindrical reactor

a) Both are governed by $\nabla^2 \phi + B^2 \phi = 0$
Both are critical. Both have same B_m^2 .
 $B_m^2 = B_g^2$ \therefore all bucklings are equal.

b) Volume of cubic reactor = H^3

$$\begin{aligned} \text{" " cylindrical reactor} &= \pi R^2 H \\ &= \pi \left(\frac{2.405}{\sqrt{2}\pi}\right)^2 H^3 = \frac{(2.405)^2}{2\pi} H^3 \\ &= 0.92 H^3 \end{aligned}$$

\therefore cylindrical reactor is smaller.

c) Power = $\underbrace{W_f \nu \Sigma_f \phi}_{\text{constant}} \times \text{Volume}$

\therefore Flux in cylindrical reactor is higher than in cubic reactor since Volume of cylinder < Volume of cube

d) Fuel burnup rate $\propto \frac{\text{interaction rate}}{\text{Volume}} \times \text{volume}$
 $= \Sigma_f \phi \times \text{Volume} \propto \text{Power}$

\therefore Fuel burnup rate = the same for both reactors.

— end —