



# ***CANDU Safety***

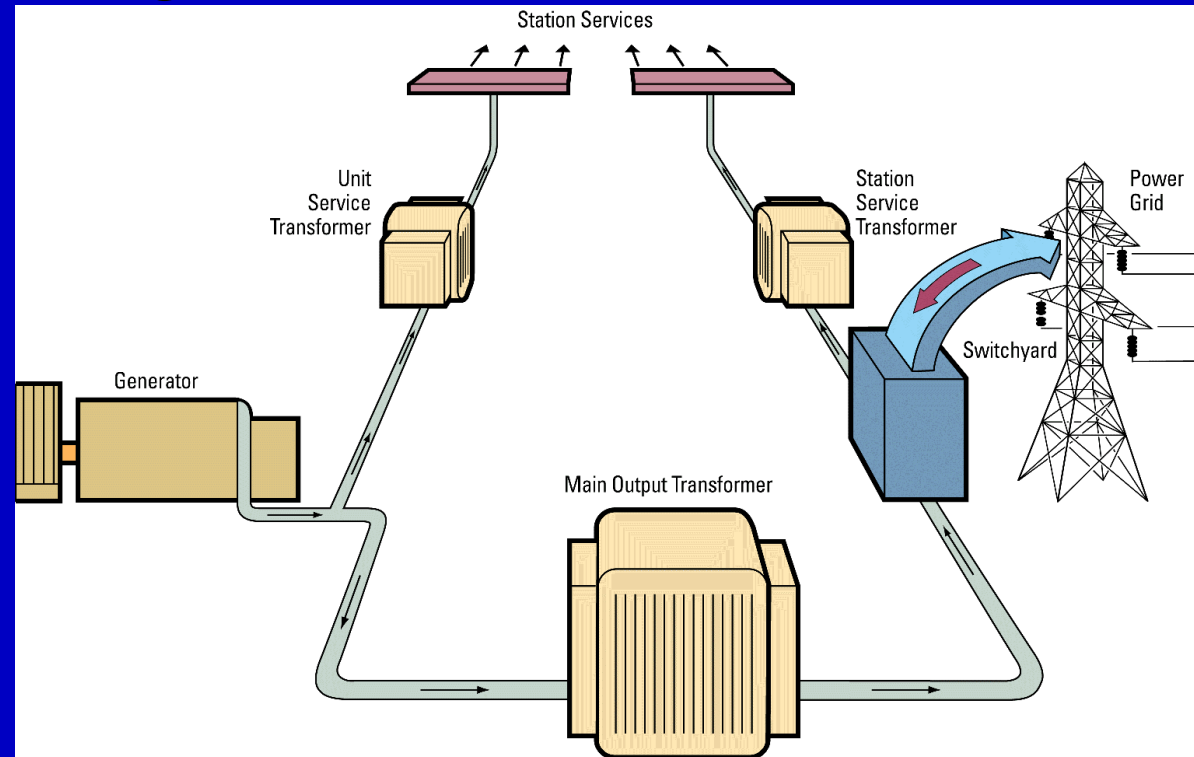
## ***#15 - Loss of Forced Circulation***

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**Director**  
**Safety & Licensing**



# Station Electrical Diagram

- λ half the station load goes directly from the unit service transformer; the other half comes from the station service transformer
- λ either can provide the total service load





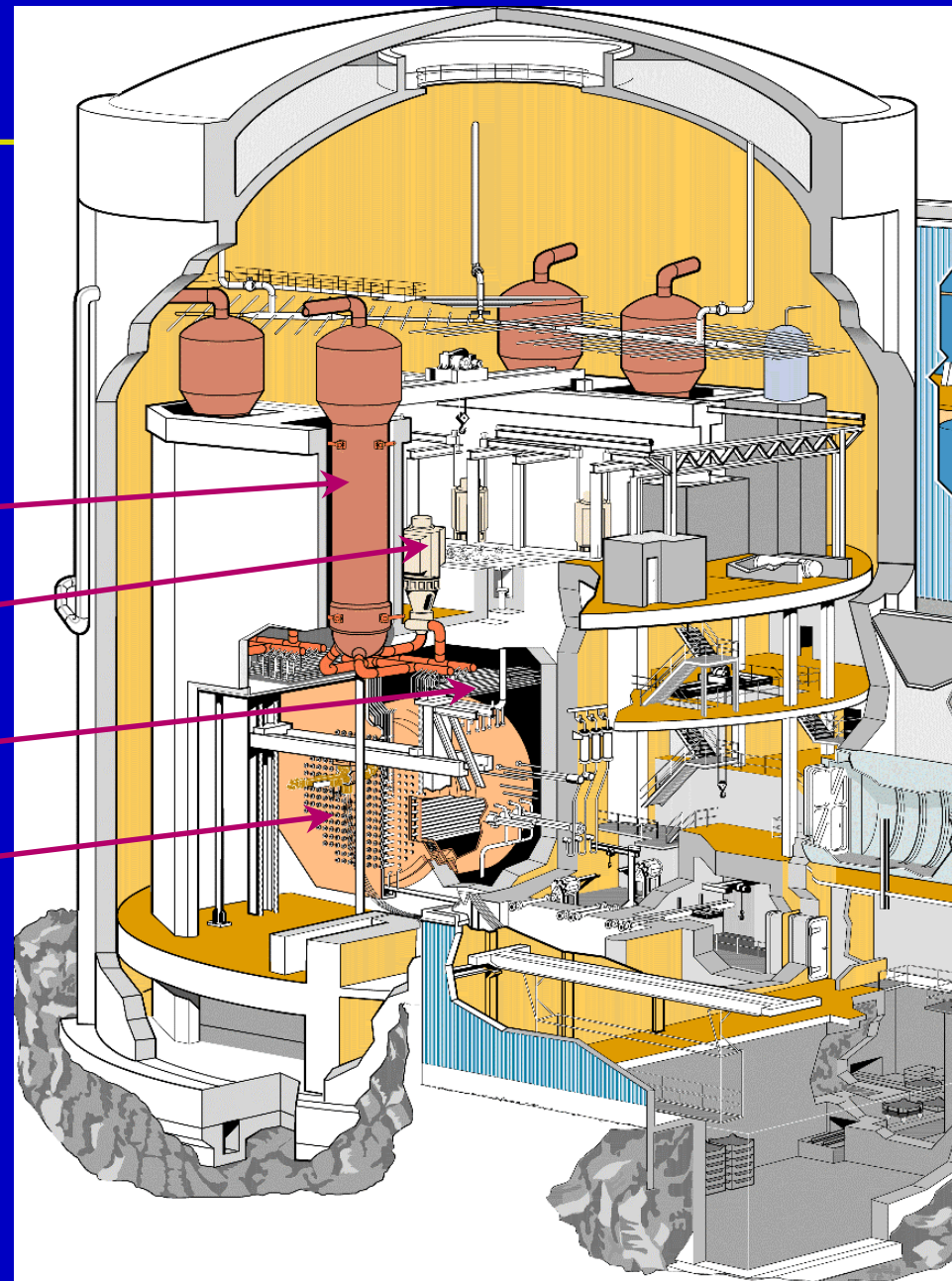
# Heat Transport System Layout

Steam generators

Main pumps

Feeder pipes

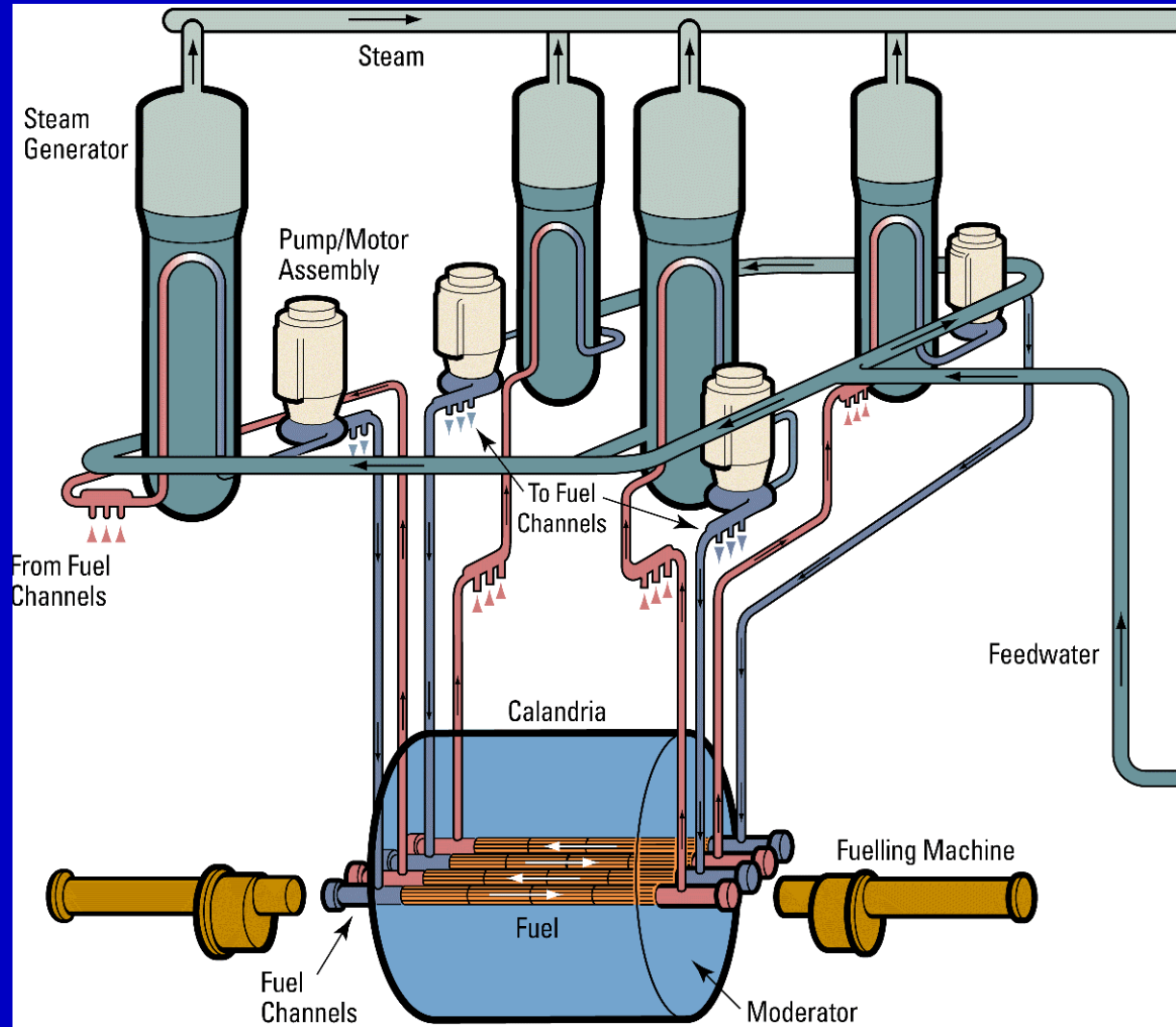
Reactor

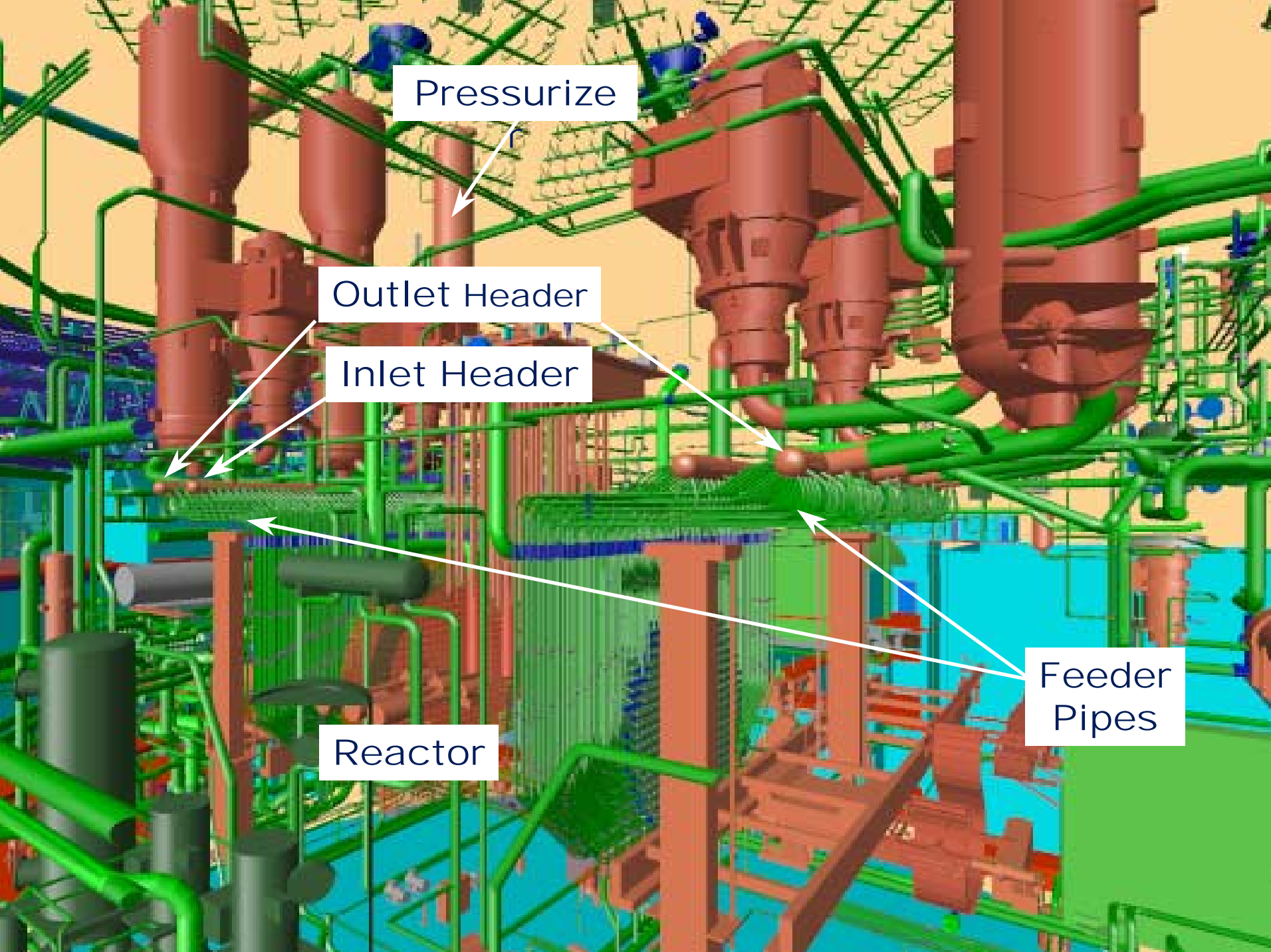




# Heat Transport System Schematic

- λ two separate heat transport system loops
- λ each has two circulating pumps *in series*
- λ steam generators located high above the core to allow for thermosyphoning if forced circulation is lost





Pressurize

Outlet Header

Inlet Header

Feeder  
Pipes

Reactor



## *Some Differences from LWRs*

- λ small power increase due to boiling in reactor core
- λ no preferred flow direction in the core
  - flow kept in “normal” direction as the pumps rundown and thermosyphoning forces take over
- λ flow is through 2 pumps and 2 steam generators in series
- λ two high-pressure long term heat sinks:
  - steam generators (auxiliary feedwater, Class III power)
  - shutdown cooling system



# *Accident Analysis - Loss of Forced Circulation*

## $\lambda$ defences

- stepback
- Shutdown System 1
- Shutdown System 2
- thermosyphoning to steam generators
- shutdown cooling system

$\lambda$  since this is an event expected one or more times in the station lifetime, stepback should be effective and prevent a trip in most cases



## *Acceptance Criteria*

- λ Class 1 Dose Limits set by AECB
- λ two effective trips on each shutdown system where practical
  - overpressure trip *only* is allowed if it is the first trip
  - prevent fuel sheath failures
  - prevent heat transport system boundary failure





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## *Cases Analyzed*

- $\lambda$  loss of Class IV power to the heat transport pumps
  - complete loss of power (4 pumps)
  - partial loss of power (2 pumps)
  - single pump trip
- $\lambda$  mechanical failure resulting in single pump seizure
- $\lambda$  various initial power levels



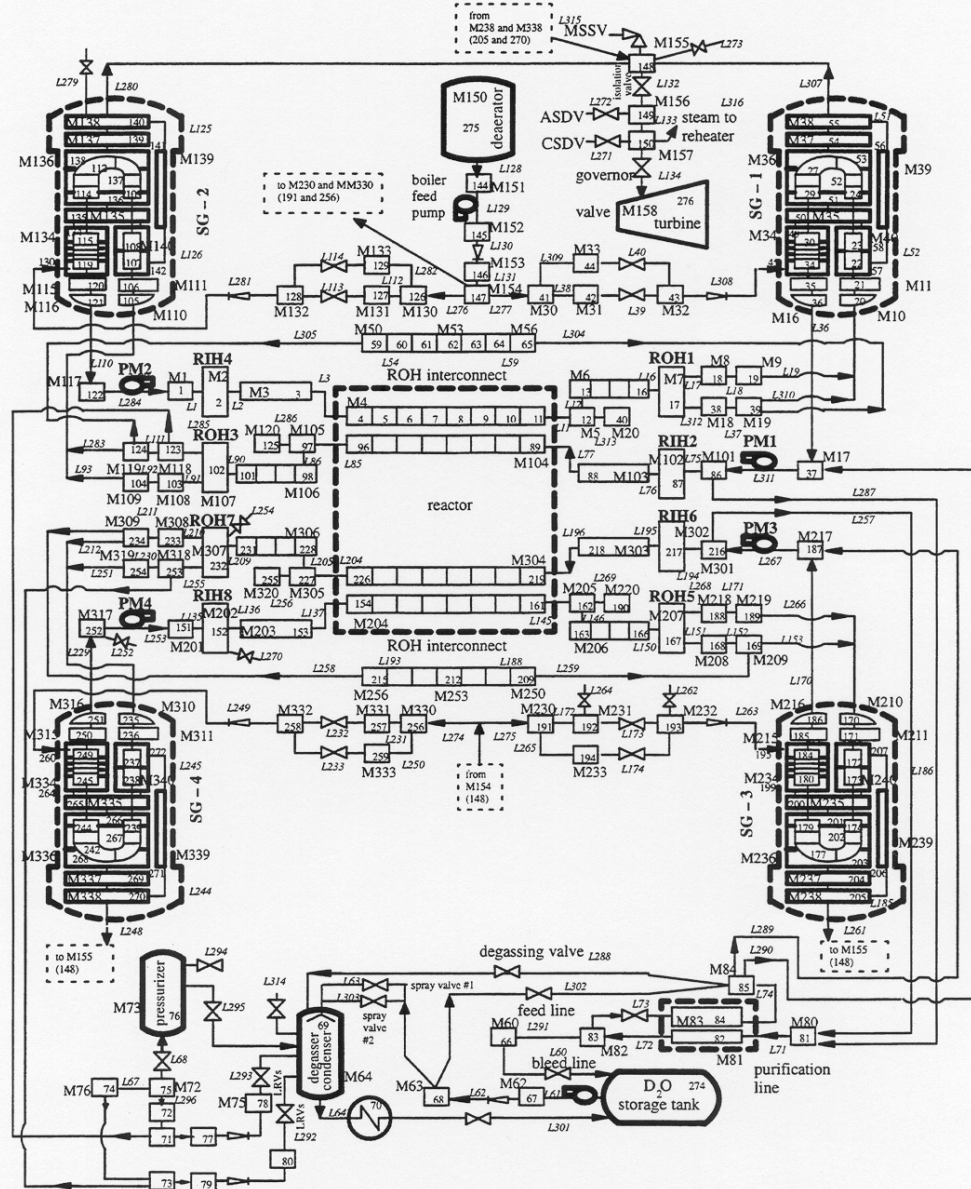
## *Relevant Trips*

High neutron power	115% full power	
Low coolant flow (SDS1)	80%	
High heat transport system pressure (immediate)	10.55 MPa	11.72 MPa
High heat transport system pressure (delayed)	10.34 MPa	
Low core pressure drop (SDS2)	450 kPa	immediate
	950 kPa	delayed



# Circuit Model

- λ the (illegible) picture at right shows the complexity of the circuit model required for trip coverage analysis
- λ the model has been compared to operating plant transients



SOPHT Two-Loop Nodalization Diagram



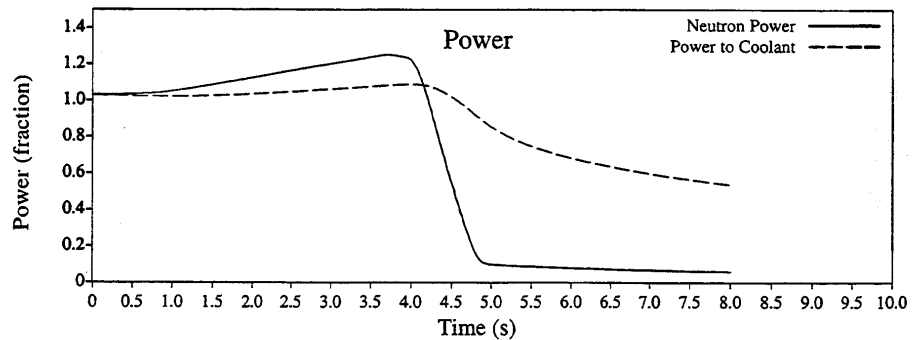
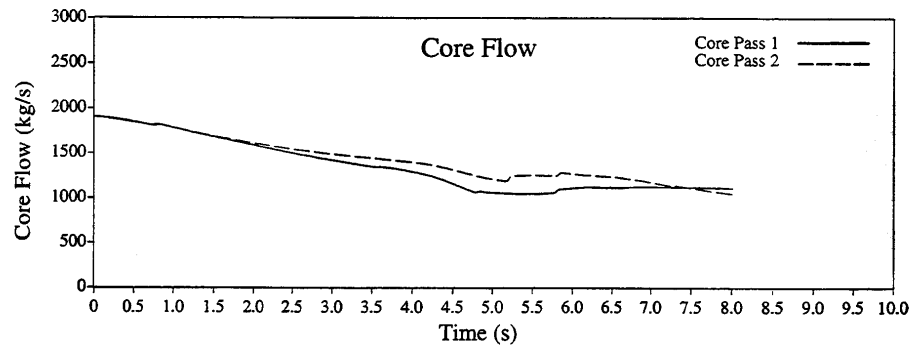
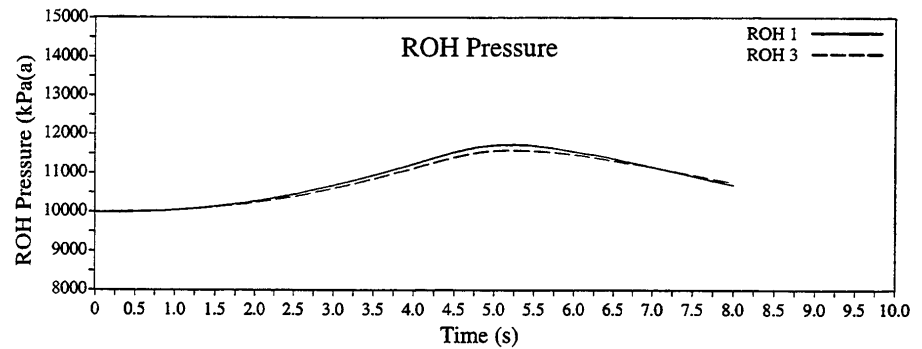
## *Event Sequence*

- λ loss of Class IV power, all pumps run down
- λ turbine trip due to loss of condenser vacuum
- λ coolant pressure increases, relief valves open, then re-close
- λ small amount of void in the core, power rises
- λ reactor shut down by stepback (not credited)
- λ reactor shut down by trip on shutdown system (s)
- λ boiler steam relief valves open, if needed, to control pressure
- λ flow matches power and heat transport system  
thermosyphons with heat being rejected to steam generators
- λ long term: use of shutdown cooling system



# Loss of Class IV from Full Power

- λ power rise due to increase in boiling in the channels, terminated by stepback or trip
- λ slow flow rundown due to high rotational inertia of the pumps

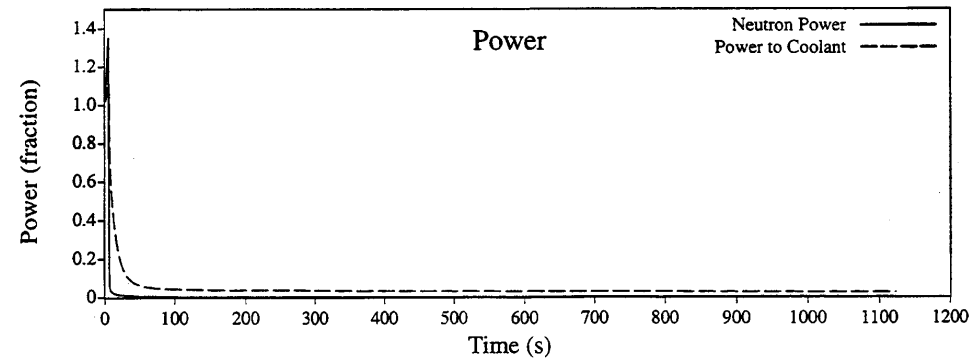
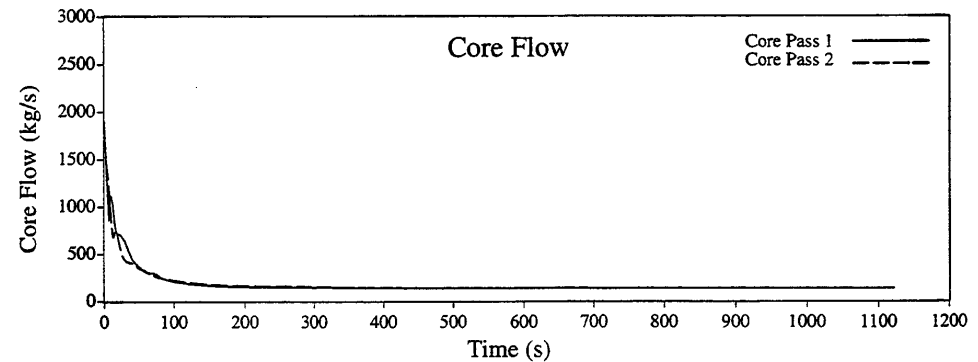
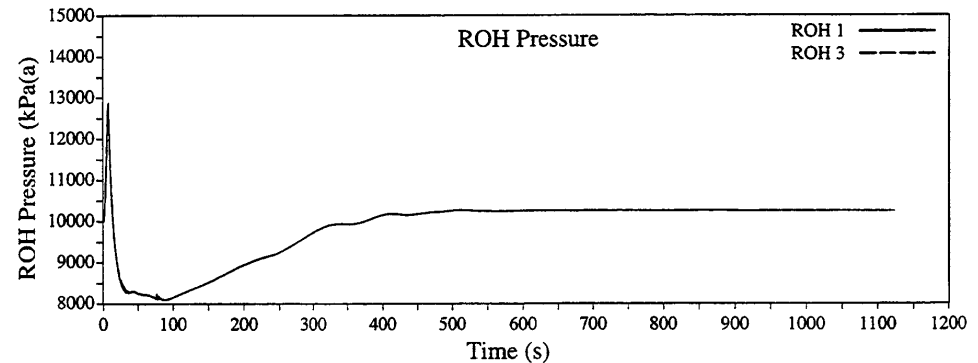


Complete Loss of Class IV Power from 103% FP,  
SDS1 High Pressure Trip



# Long Term Behaviour

- λ flow rundown to match reactor decay power
- λ reactor outlet header pressure rises to reject heat to steam generators

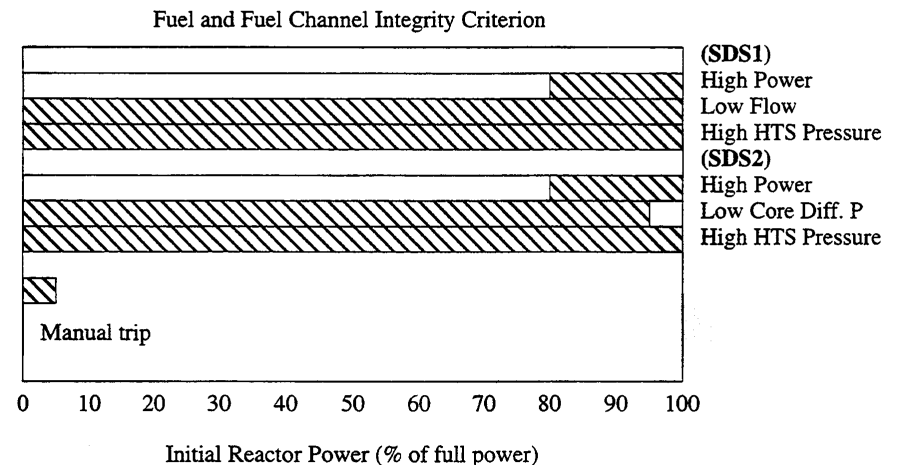
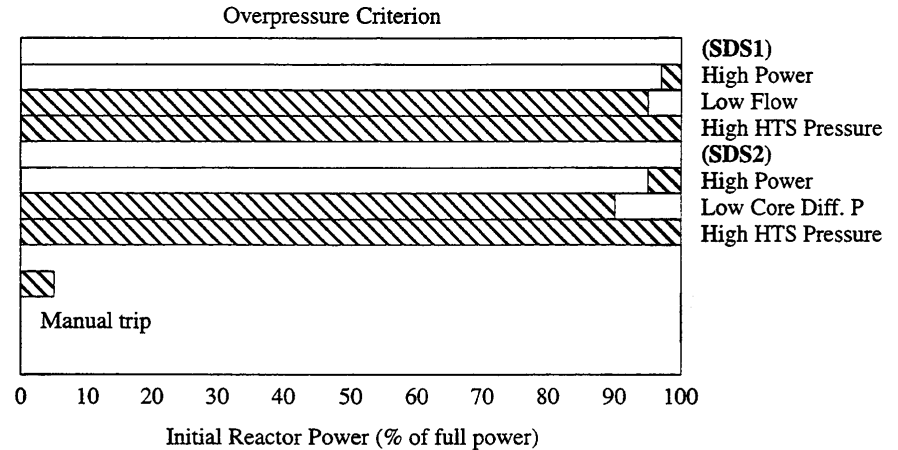


Complete Loss of Class IV Power from 103% FP, Trip on SDS2 High Pressure, Long Term Thermosyphoning



# Trip Coverage Maps

- λ at least 2 effective trips for fuel protection
- λ two effective trips in most cases to meet acceptance criteria for overpressure
- λ limited area of single trip coverage on *each* shutdown system
  - sometimes only a high pressure signal is effective in detecting high pressure



Note: SDS1 Low Flow conditioned out below 0.1 % FP  
SDS2 Low Core Differential Pressure conditioned out below 5% FP

Trip Coverage Map for Complete Loss of Class IV Power  
(Fresh or Equilibrium Fuel and Fouled Steam Generators) RRS Frozen



## *Other Events - Moderator Pipe Rupture*

- $\lambda$  low pressure piping
- $\lambda$  issues
  - release of tritium
  - increase in deuterium gas concentration in cover gas
- $\lambda$  power reduction on Regional Overpower Protection System trip (high local powers) or “naturally” as moderator level falls





## *Other Events - Fuel Handling Failures*

- λ can affect at most one channel plus fuel in fuelling machine
- λ separate D<sub>2</sub>O cooling system when off-reactor
- λ examples:
  - loss of cooling to fuelling machine off-reactor
  - fuelling machine detaches from channel without replacing closure plug
- λ safety case bounded by single channel events
- λ large heat capacity in fuelling machine slows down the heat-up of the fuel



## *Summary*

- λ geometrical layout of CANDU is favourable to thermosyphoning
- λ slow power rise stopped by regulating or shutdown systems
- λ flow direction stays the same
- λ two high-pressure heat sinks
- λ can reject heat to feeders in the very long term, with no preferred flow direction in the channels