



CANDU Safety #8 - Containment

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What's Special About CANDU Containment?

- λ not much
- λ containment type is not tied to the CANDU design:
 - single unit pressure suppression (CANDU 6)
 - multi-unit vacuum pressure suppression (Ontario Hydro)
 - double containment with suppression pool (recent Indian HWRs)
 - single-unit dry (CANDU 9)



Single Unit Pressure Suppression (CANDU 6)



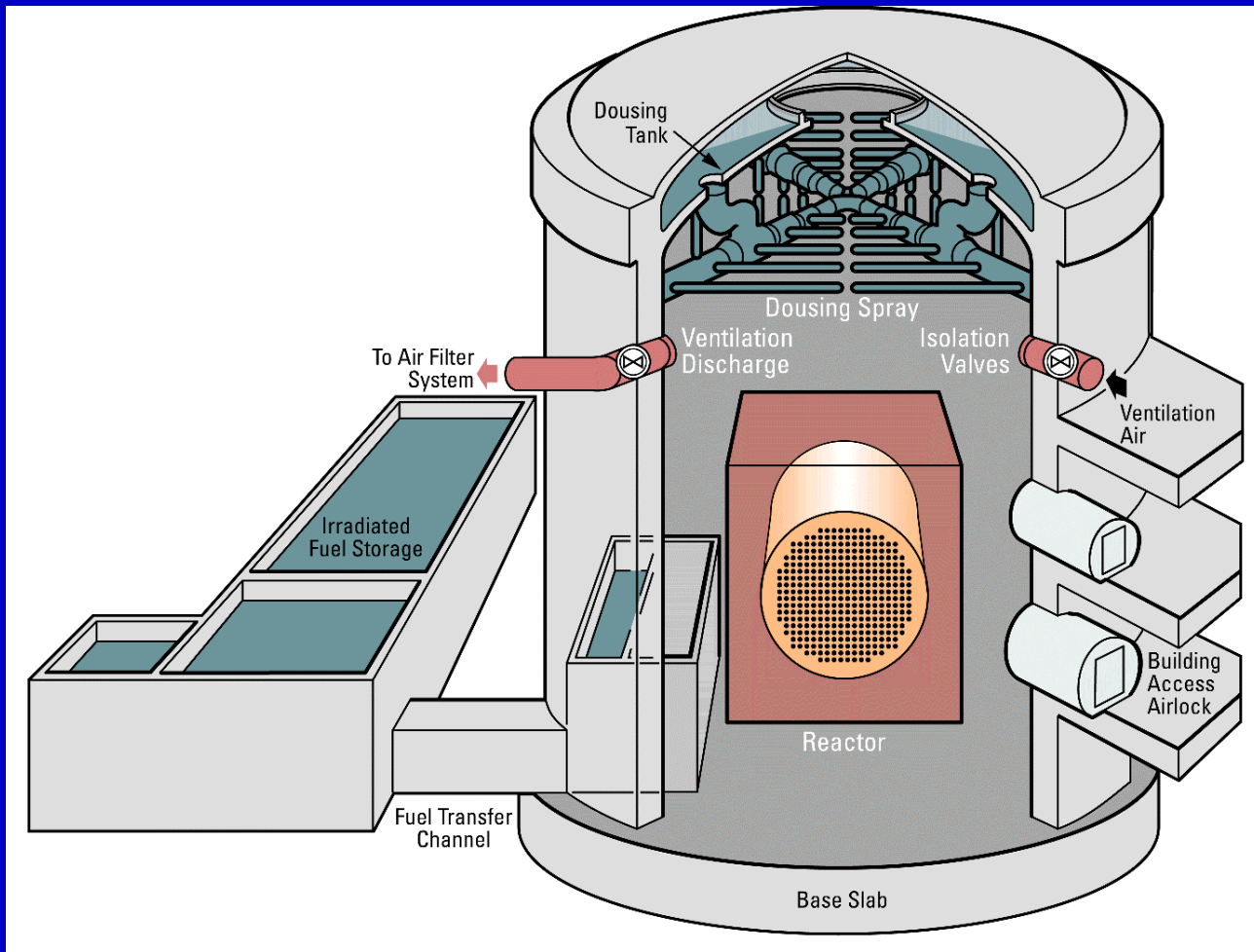


Fundamental Requirements

- λ design pressure set above pressure reached in large LOCA
- λ leak rate at design pressure set to ensure the dose to the public in an accident is less than the regulatory limit
- λ note that the dose is *calculated* from:
 - release to containment using physically-based models of reactor physics, fuel, reactor thermohydraulics, etc.
 - containment pressure transient using physically-based models of containment thermohydraulics
 - atmospheric dispersion models



Single-Unit Pressure Suppression





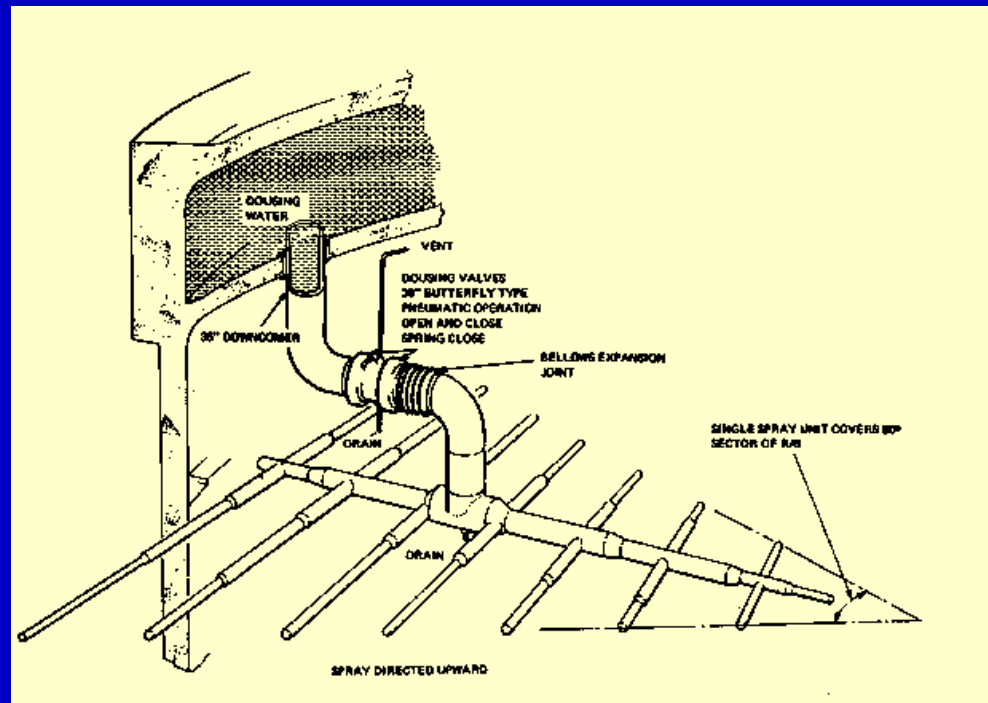
Design Summary - CANDU 6

- λ prestressed, post-tensioned concrete structure
 - keeps the building in compression
- λ relatively *large*
 - 41 metres ID × 44 metres high; 48,000 m³ net volume
 - diameter required for fuelling machines
 - large volume per unit energy allows lower design pressure (124 kPa (g))
- λ wall thickness: 1.1 metres
- λ walls lined with epoxy for leak-tightness
- λ design leakrate: 0.5% / day at design pressure



Dousing

- λ powerful pressure suppression, *not* like LWR sprays
- λ in elevated tank around building dome
- λ capacity 1560 m³, flowrate 4500 kg/sec for 4 out of 6 headers





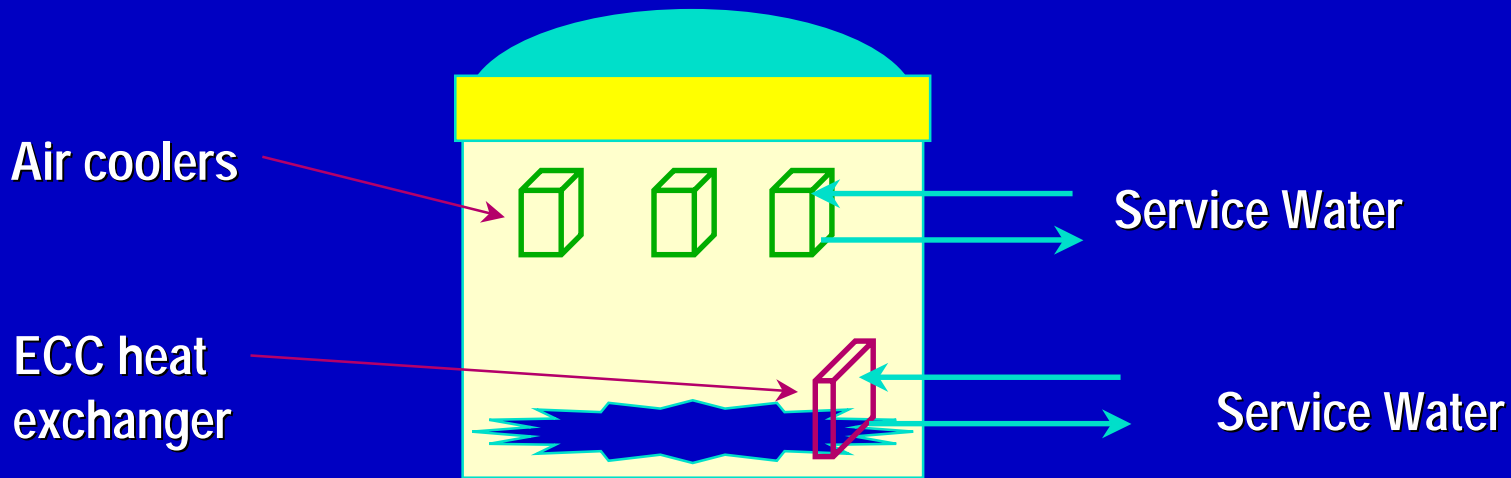
Dousing Operation

- λ 6 spray headers, each with 2 valves in series (to avoid inadvertent douse, which is costly)
- λ dousing turns on when building pressure reaches 14 kPa (g) and off if it falls to 7 kPa (g)
 - always on for large LOCA until dousing water is all used
 - cycles on & off for small LOCA
- λ dousing connections above bottom of tank so 500 m³ of water is reserved for medium-pressure ECC
- λ assists in fission product washout
- λ no effect in long-term containment pressure control



Long-Term Cooling

- λ 16 local air coolers
- λ condensation on structures and equipment
- λ for LOCA, emergency core cooling system heat exchangers





Ventilation

- λ in operation, most of the containment building is accessible, unlike most LWRs
- λ ventilation is needed for working conditions and to control and condense heavy water vapour
- λ on a containment isolation signal (high pressure or high radiation), redundant valves in each ventilation line to the atmosphere are closed - but *not* major process lines
- λ unavailability of ventilation valve closure must be $< 10^{-3}$ as with other safety systems
- λ tested during operation to show the unavailability target is not exceeded



Hydrogen Control

- λ hydrogen can build up:
 - in the short term, from clad oxidation, in a severe accident such as a LOCA + Loss of Emergency Core Cooling
 - in the long term, after a LOCA, due to radiolysis
- λ natural circulation in containment and the size of the building reduces the hydrogen concentration for LOCA + LOECC
- λ forced flow from Local Air Coolers mixes hydrogen
- λ supplemented by 44 igniters to ignite local concentrations
- λ for “worst” LOCA + LOECC, maximum room hydrogen concentration is 7%; building average is 3.5%



Acceptance Criteria

- λ peak pressures must be less than design pressure for:
 - 1. LOCA**
 - 2. LOCA with loss of emergency core cooling**
 - 3. LOCA with loss of all dousing****
- λ there must be no structural failure which could damage the reactor systems for:
 - 4. steam or feedwater line break**
 - 5. steam or feedwater line break with loss of all dousing****
- λ there must be no damage to the containment structure for items 1 to 4**



Discussion of Design Pressure

- λ containment pressure must be less than design for accidents which can release fission products
- λ this includes some *severe accidents* such as LOCA + LOECC
- λ containment leakage is not as important for accidents which do not release much radioactivity (and steam line breaks cause a power reduction, not an increase)
- λ the structural integrity of the building must be maintained even for some multiple failures



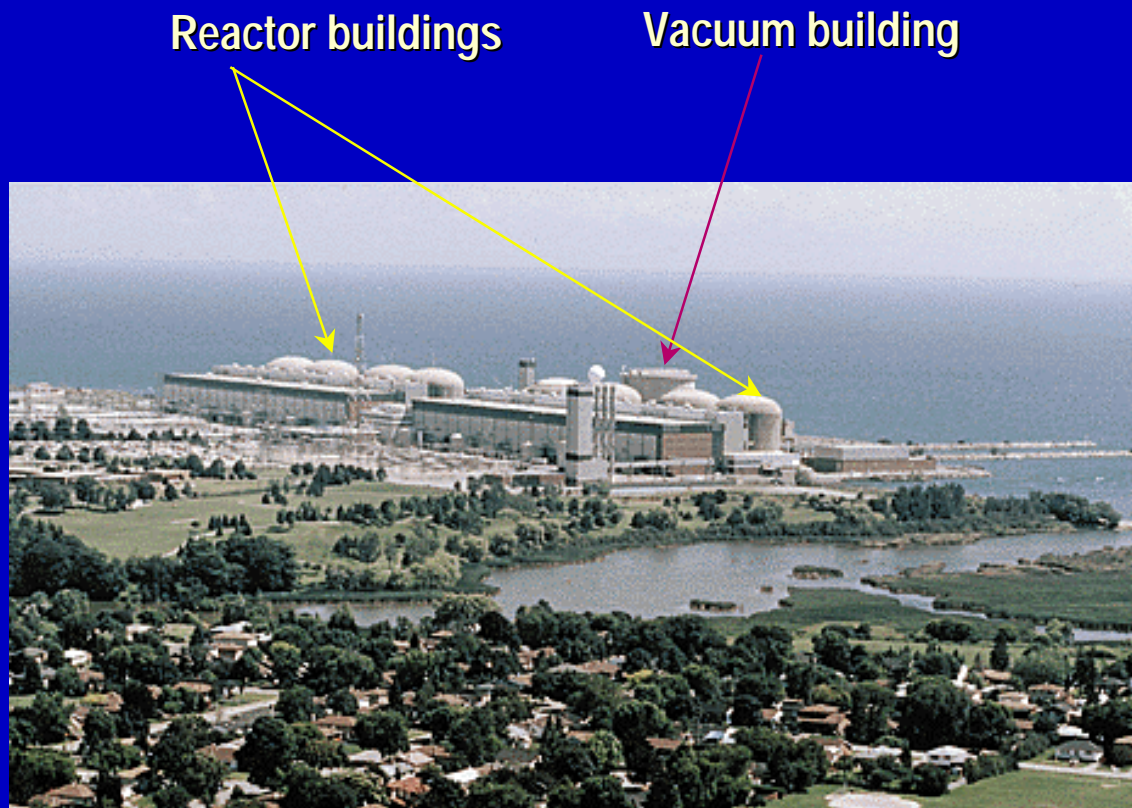
Overpressure Behaviour

- λ in severe accidents which increase pressure far beyond design pressure, failure mode is “graceful”
 - increasing leakage through cracks
 - no massive failure
- λ AECB tests on scaled model CANDU 6 containment
 - through-wall cracks at 2.7 times design pressure, negligible leakage
 - failure at 4.3 times design pressure *if* pressure could be maintained
 - leakage rate increases rapidly and prevents failure



Multi-Unit Vacuum Containment

- λ each reactor containment is connected by a large duct to a common vacuum building
- λ water sprays in vacuum building condense steam
- λ containment stays subatmospheric for days after an accident so the leakage is inward
- λ very powerful and allowed siting of CANDUs near major city (Toronto)



Pickering 8-Unit CANDU, near Toronto



Single Unit Dry Containment

- λ CANDU 9
- λ dousing has been removed
- λ higher containment design pressure
- λ steel-lined for increased leak-tightness

